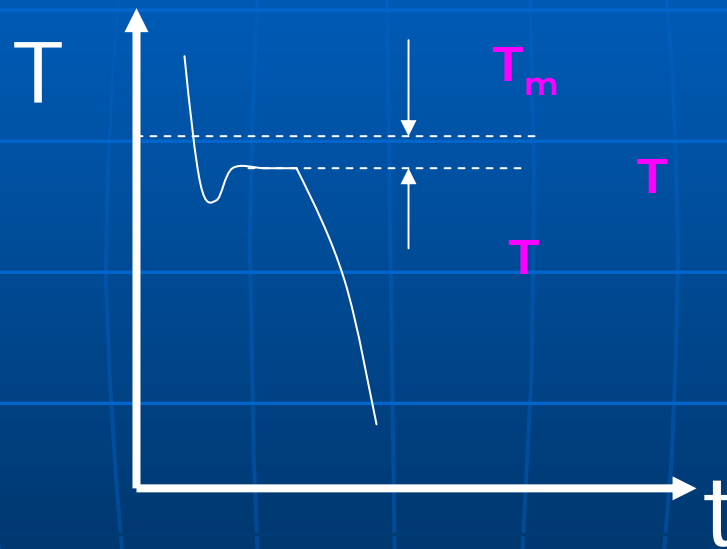


1



冷却过程中的结晶温度
平衡状态时的结晶温度

T
 T_m

$$T = T_m - T$$

.

$$G_S - G_L = \Delta G < 0$$

$$S > 0$$

T

$$S_L > S_S$$

$$G = H - TS$$

$$G \quad T$$

$$\frac{dG}{dT} = -S$$

$$G_L - T$$

$$G_S - T$$

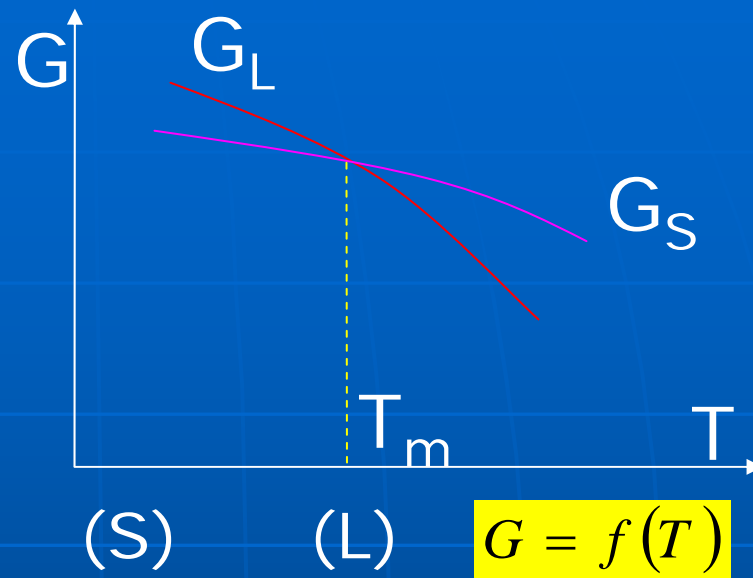
$$T_m$$

$$G_L = G_S$$

$$G_S - G_L = G < 0$$

$$T < T_m$$

G



$$\Delta G = G_S - G_L = (H_S - H_L) - T(S_S - S_L),$$

$$H_S - H_L = -L_m; S_S - S_L = -\Delta S_m = -L_m / T_m$$

$$\Delta G = -L_m \Delta T / T_m$$

1.

2.

3.

4.

5.

:

1.

(1).

:

G_V

$$\Delta G = V \bullet \Delta G_V + A \bullet \sigma$$

$$= -\frac{4}{3}\pi r^3 \bullet \Delta G_V + 4\pi r^2 \bullet \sigma$$

$$: \quad G' = -4 \pi r^2 \bullet \Delta G_V + 8 \pi r \bullet \sigma = 0$$

$$r = \frac{2\sigma}{\Delta G_V}$$

r_c

$$\begin{aligned}
 \Delta G_c &= -\frac{4}{3}\pi \cdot r^3 \cdot \Delta G_V + 4\pi \cdot r^2 \cdot \sigma \\
 &= -\frac{4}{3}\pi \cdot \left(\frac{2\sigma}{\Delta G_V}\right)^3 \cdot \Delta G_V + 4\pi \cdot \left(\frac{2\sigma}{\Delta G_V}\right)^2 \cdot \sigma = \frac{16\pi \cdot \sigma^3}{3\Delta G_V^2} \\
 &= 4\pi \cdot r^2 \cdot \frac{\sigma}{3} = \frac{A \cdot \sigma}{3}
 \end{aligned}$$

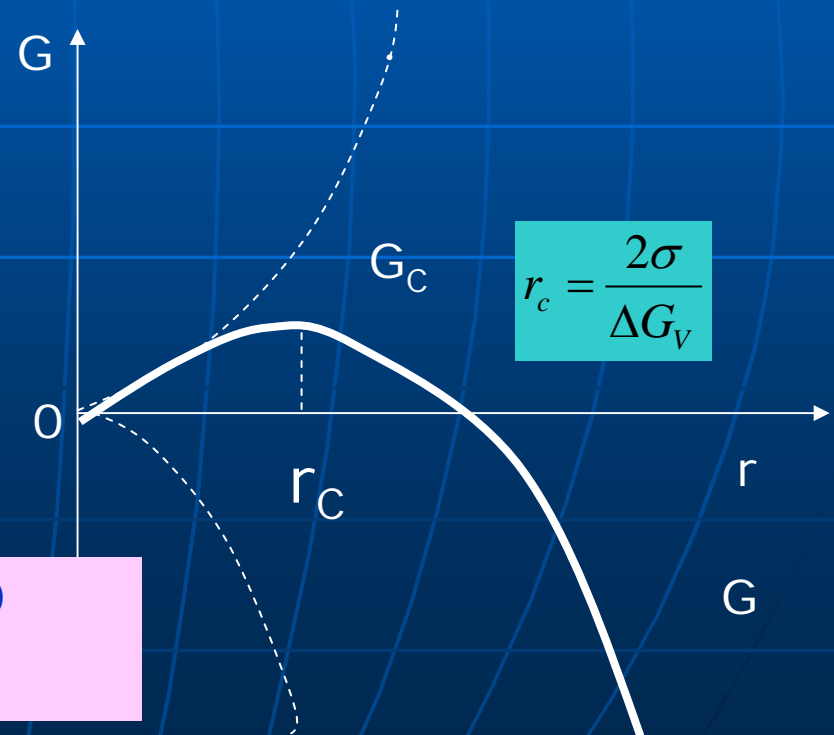
$$G = H - TS,$$

$$G = 0, \quad S = H/T_0,$$

$$\Delta G_V = \Delta H - \frac{T\Delta H}{T_0} = \frac{\Delta H}{T_0}(T_0 - T)$$

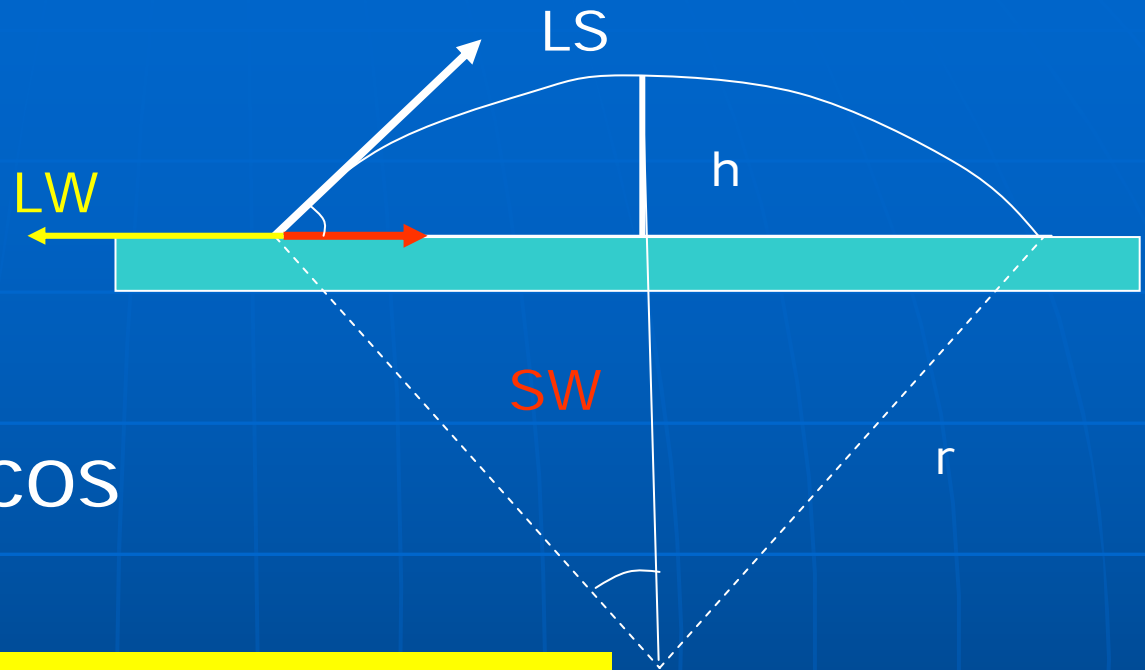
讨论:

- 1) $T = T_m$, 不成核;
- 2) $\Delta T > 0$, 必要条件;
- 3) $r_n > r_c$, 核长大.



$$\begin{aligned}
 T & 0.2T_m, \quad 150 \sim 250 \\
 & < 20
 \end{aligned}$$

(2).



$$LW = SW + LS \cos \theta$$

$$V_s = \frac{\pi r^3}{3} (2 - 3 \cos \theta + \cos^3 \theta)$$

$$A_{SL} = 2\pi r h = 2\pi r (r - r \cos \theta) = 2\pi \cdot r^2 (1 - \cos \theta)$$

$$SW = \rho \cdot V_s = \rho \cdot \frac{\pi r^3}{3} (2 - 3 \cos \theta + \cos^3 \theta)$$

$$G_{LW} = V_S \cdot G_V + A_{LS} \cdot \sigma_{LS} + A_{SW} \cdot \sigma_{SW}$$

$$= \frac{\pi \cdot r^3}{3} (2 - 3 \cos \theta + \cos^3 \theta) \cdot \Delta G_V$$

$$\Delta G = \left(-\frac{4}{3} \pi \cdot r^3 \cdot \Delta G_V + 4 \pi \cdot r^2 \cdot \sigma \right) \cdot \frac{(2 + \cos \theta)(1 - \cos \theta)^2}{4}$$

$$= G_C \cdot f$$

$$f = \frac{(2 + \cos \theta)(1 - \cos \theta)^2}{4}$$

$$r_c^* = \frac{2 \sigma_{SL}}{\Delta G_V}$$

$$G = G_c \cdot f$$

讨论

1. $\theta = 0^\circ$, $G = G_c$, $f = 1$



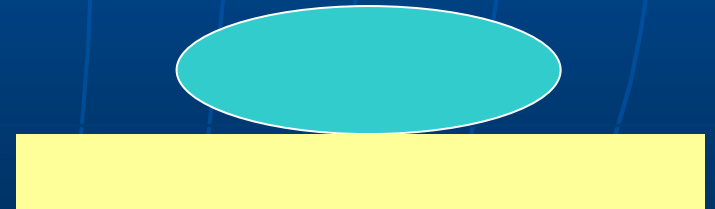
2. $\theta = 90^\circ$, $G = G_c/2$, $f = 1/2$

$$f = \frac{(2+0)(1-0)^2}{4} = \frac{1}{2}$$



3. $\theta = 180^\circ$, $G = G_c$, $f = 1$

$$f = \frac{(2-1)(1+1)^2}{4} = 1$$



(3).

N

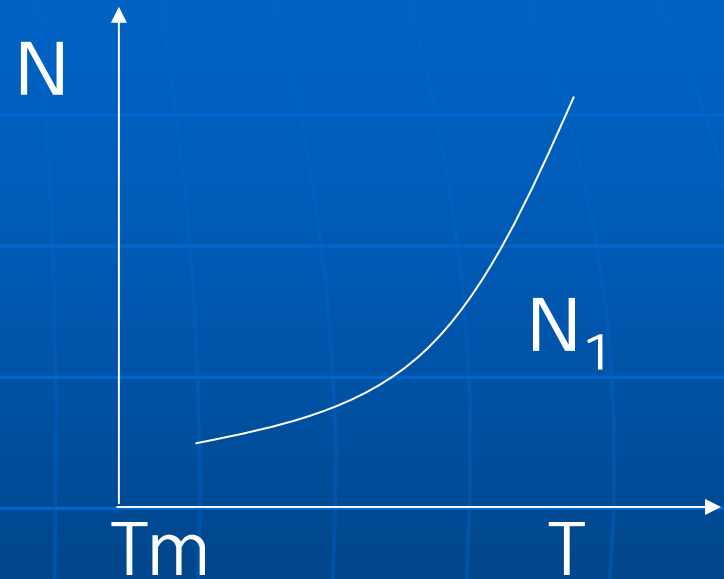
/cm³.sec

n rc
 N , :

$$\frac{dn}{N} = -\frac{\Delta G}{k \cdot T},$$

$$\int_n^N \frac{dn}{n} = \ln \frac{n}{N} = -\frac{\Delta G}{kT}$$

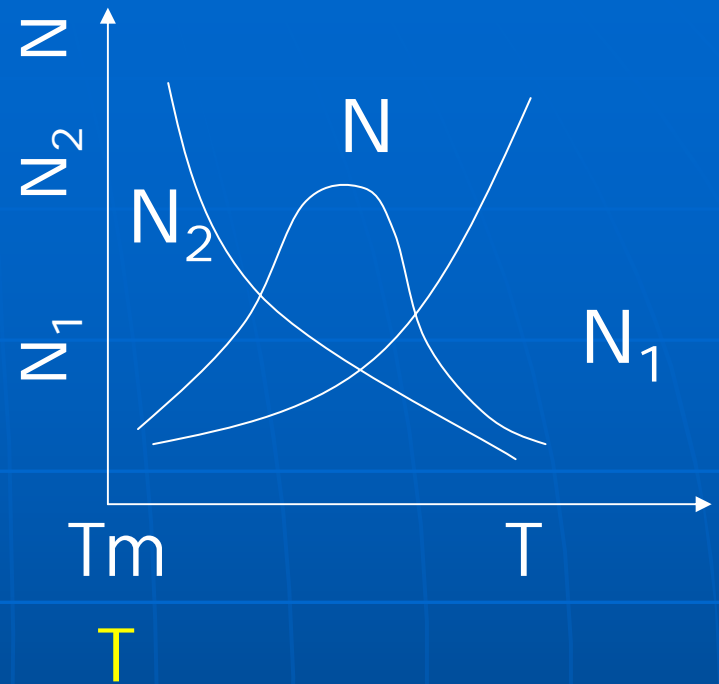
$$\frac{n}{N} = e^{-\frac{\Delta G}{kT}} \quad K$$



T

r_c G_c T

$$N_1 \propto \exp(-\Delta G_c / (kT))$$



b

$$N_2 \propto \exp(-Q / (kT))$$

N:
$$N = N_1 \cdot N_2 = K \exp(-\Delta G_c / (kT)) \cdot \exp(-Q / (kT))$$

2.

(1).

G_s

x

$$\Delta G_s / (NkT_m) = ax(1-x) + x \ln x + (1-x) \ln(1-x)$$

K:

T_m

=

S_m/R

J

ckson

,

S_m

,

R

$v(Z)$

=

$/v$

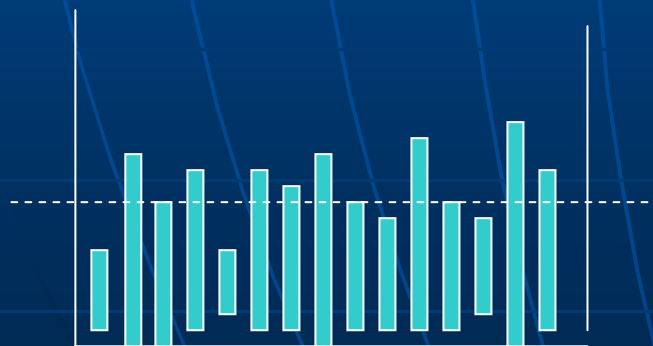
$$\left(\frac{G_s}{NkT_m} \right) \times 3$$

I.

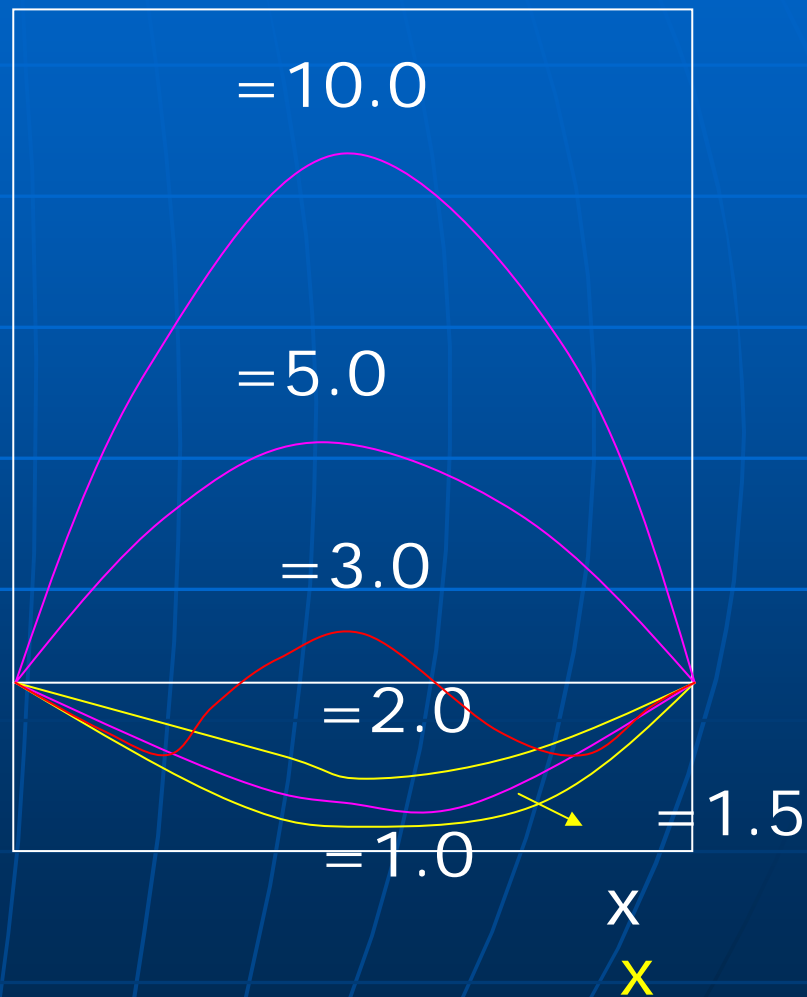
2

:

,



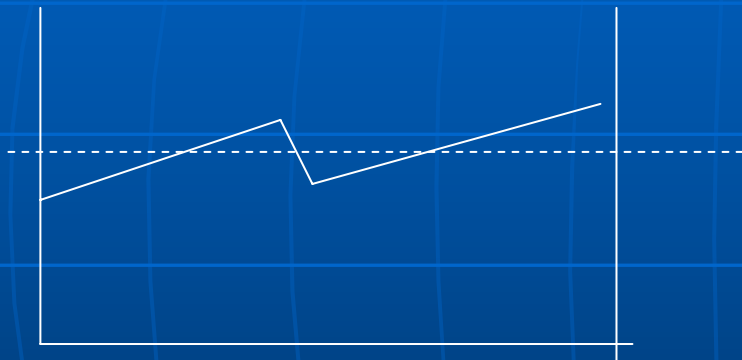
$G_s/(NkT_m)$



II.X

0.5

x 0 x 1

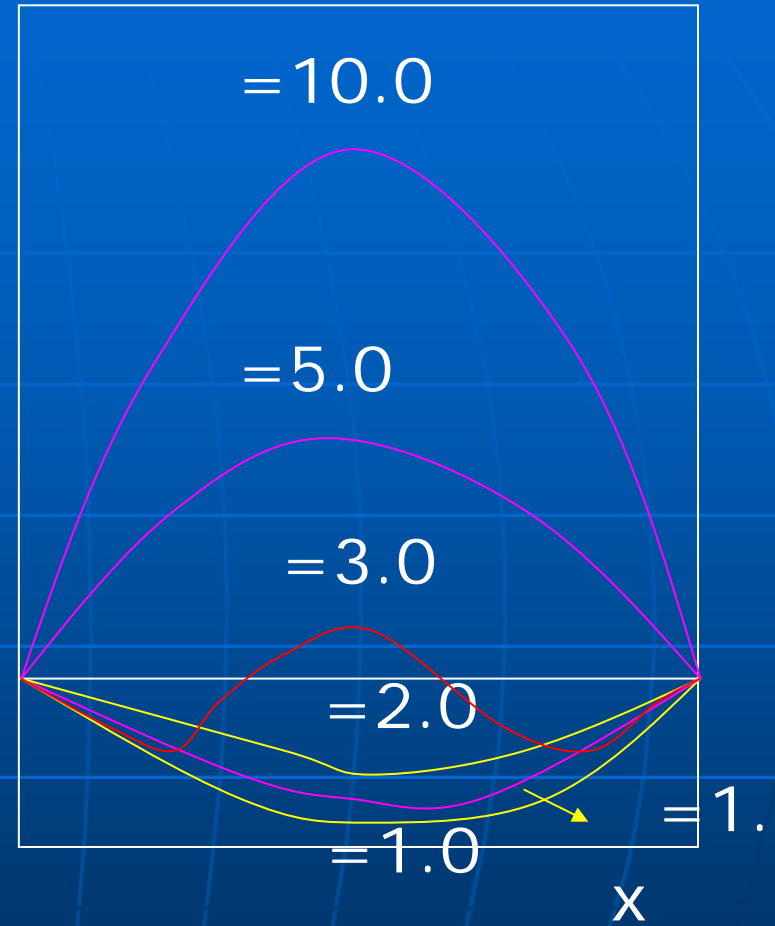


:

.

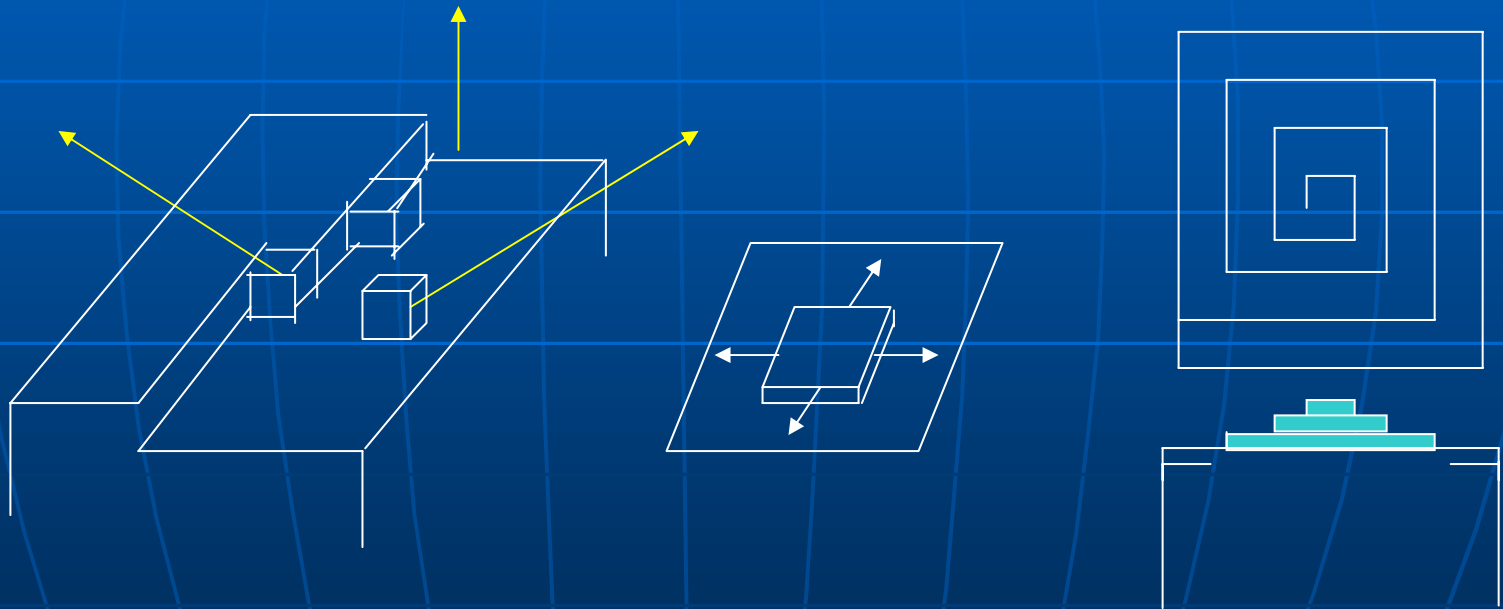
, Ge, Si

$G_s/(NkT_m)$



(2).

. ()



R:

T_k

$$R = \mu_2 \exp[-b / \Delta T_k], \Delta T_k = 1-2^\circ C$$

:

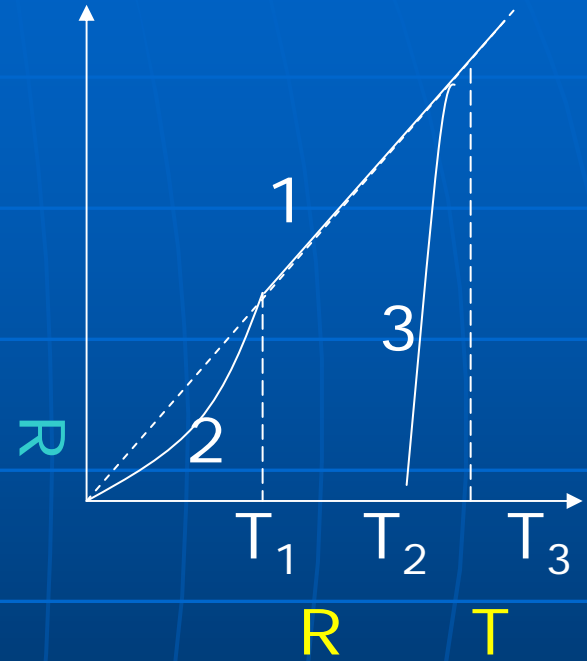
$$R = \mu_3 \Delta T_k^2$$

μ_3

b. ()

T_k

$$R = \mu_1 \Delta T$$

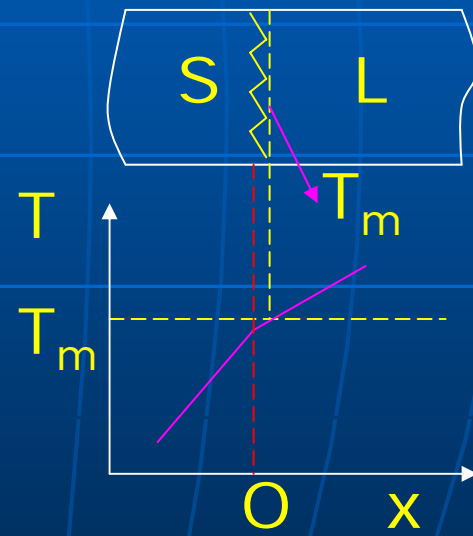
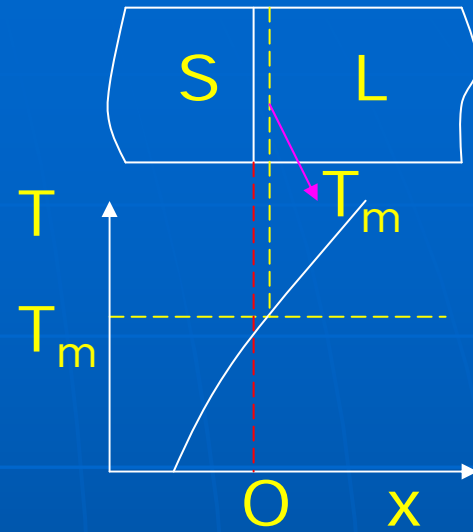
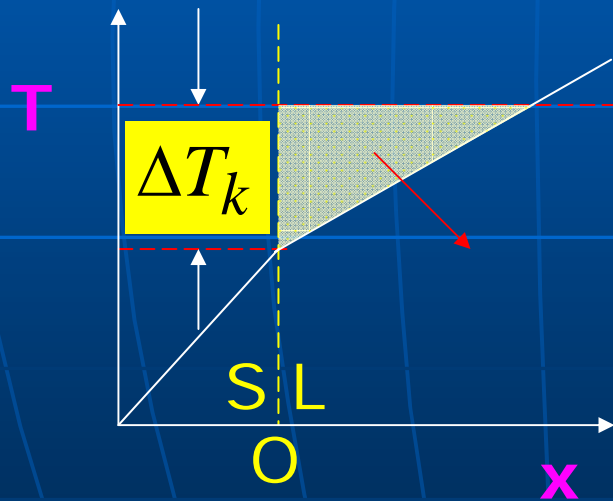


1-

2-

3-

(3).



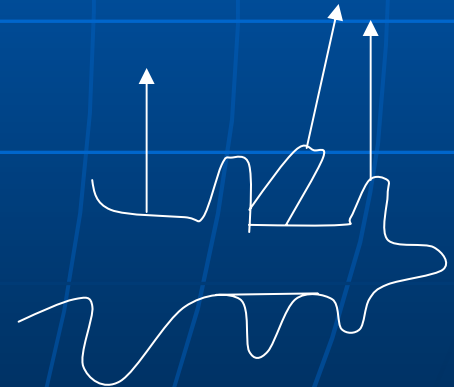
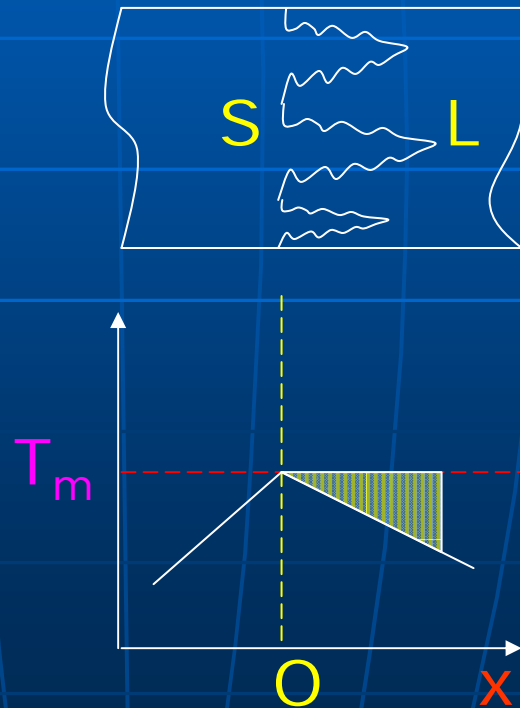
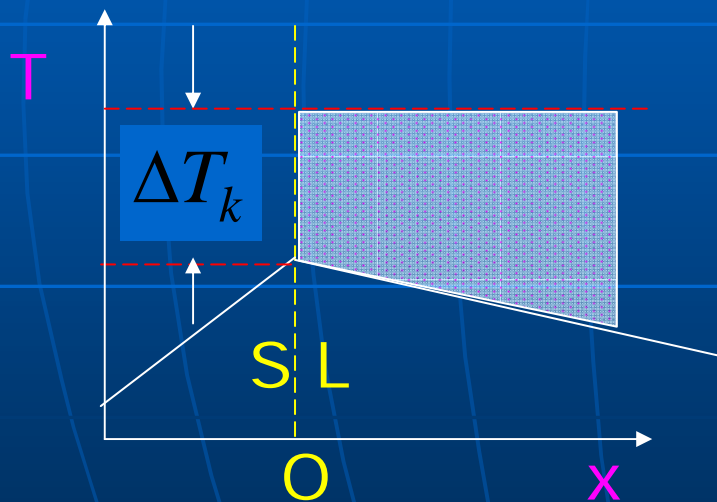
$$G_L = dT / dx > 0$$

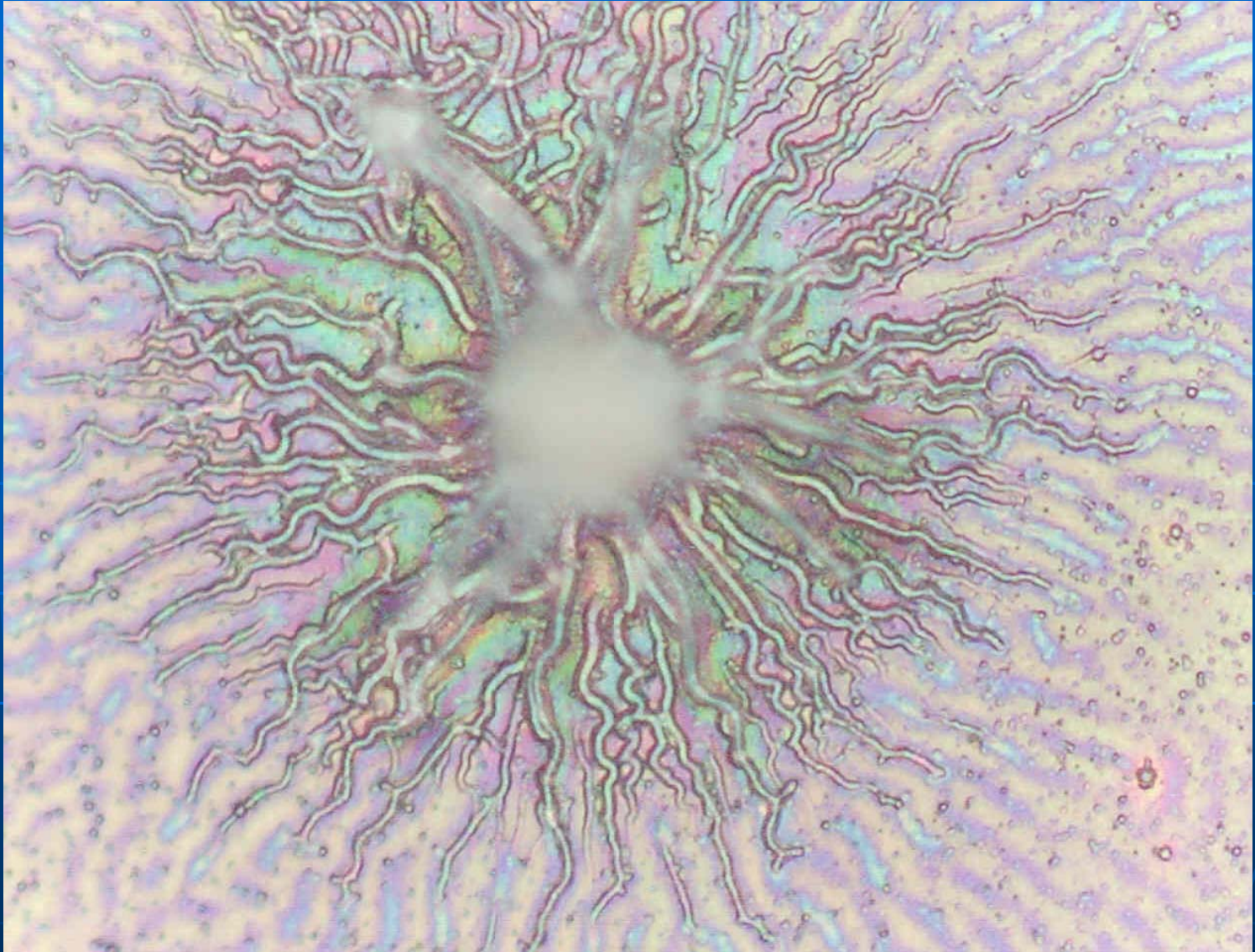
T_k

(x)

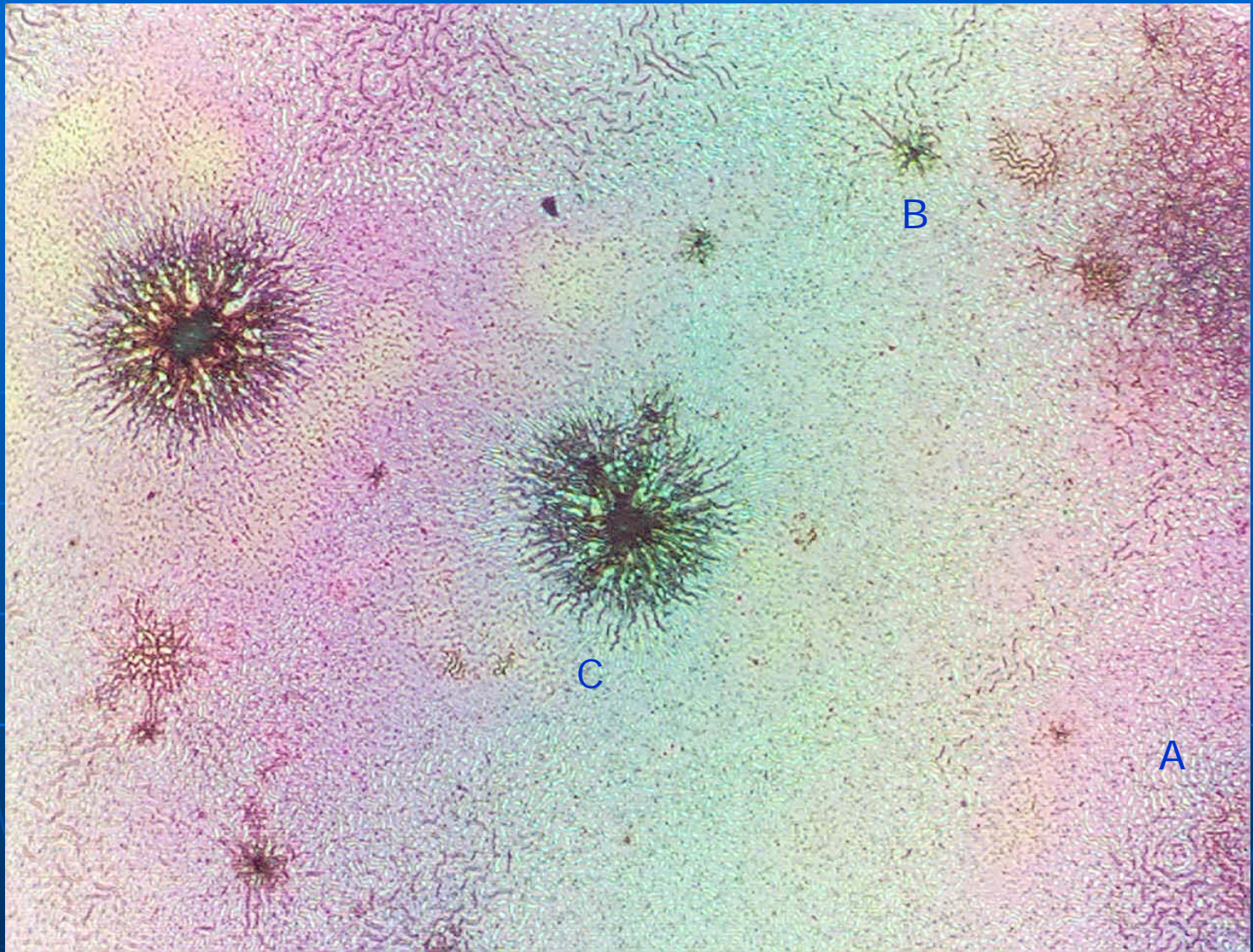
b.

$$G_L = dT / dx < 0$$





ZnO



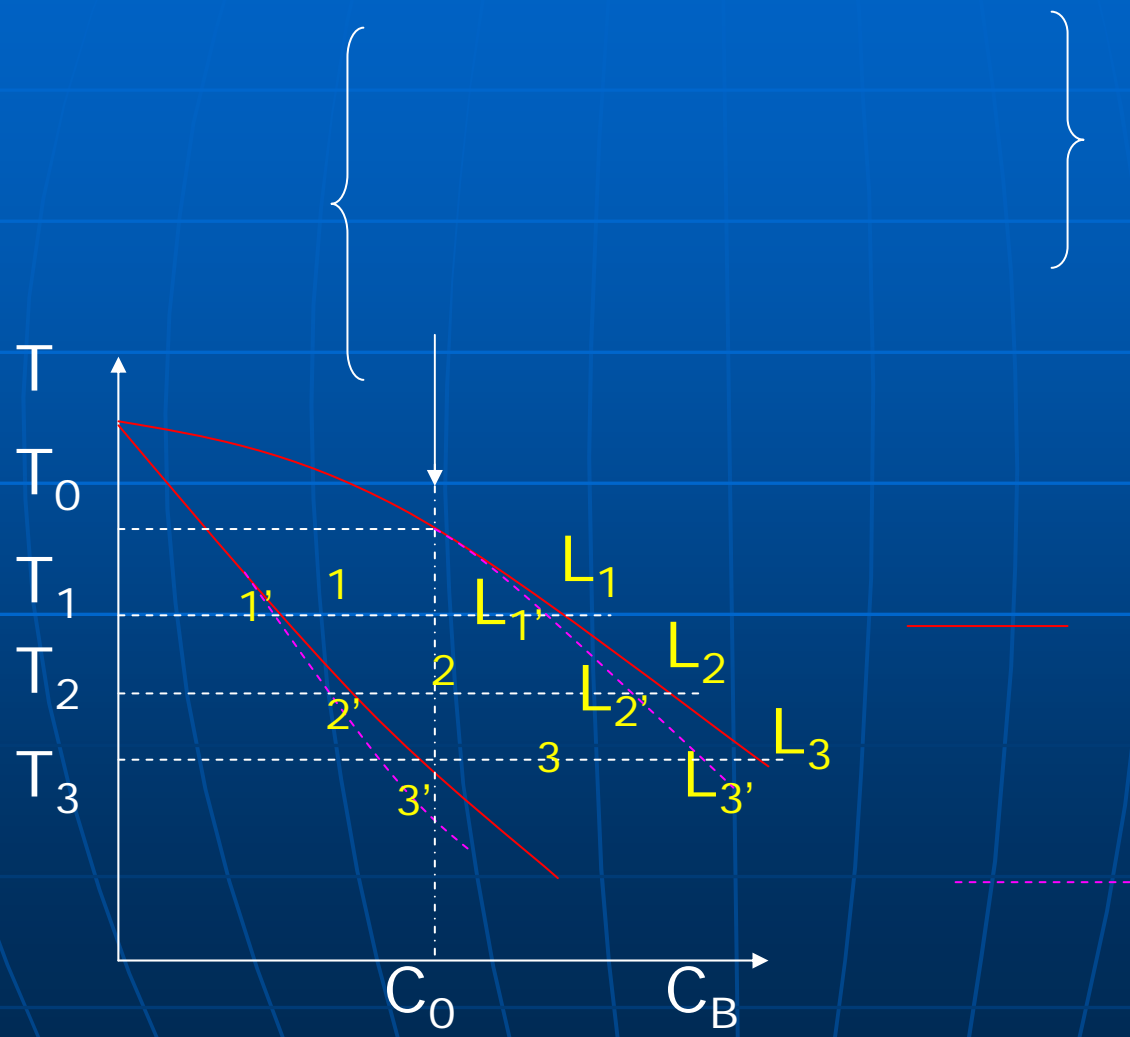
ZnO

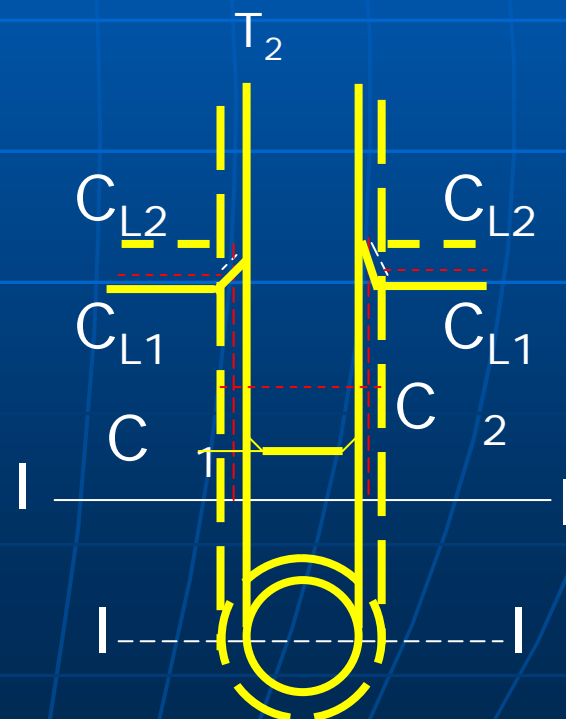
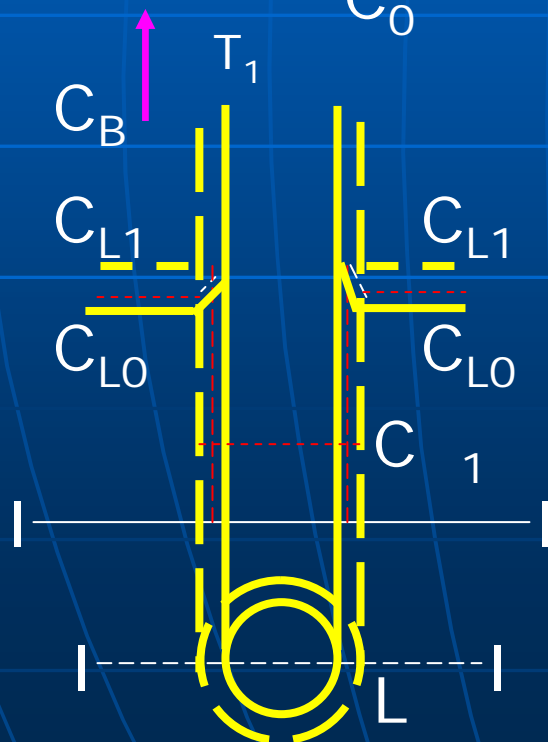
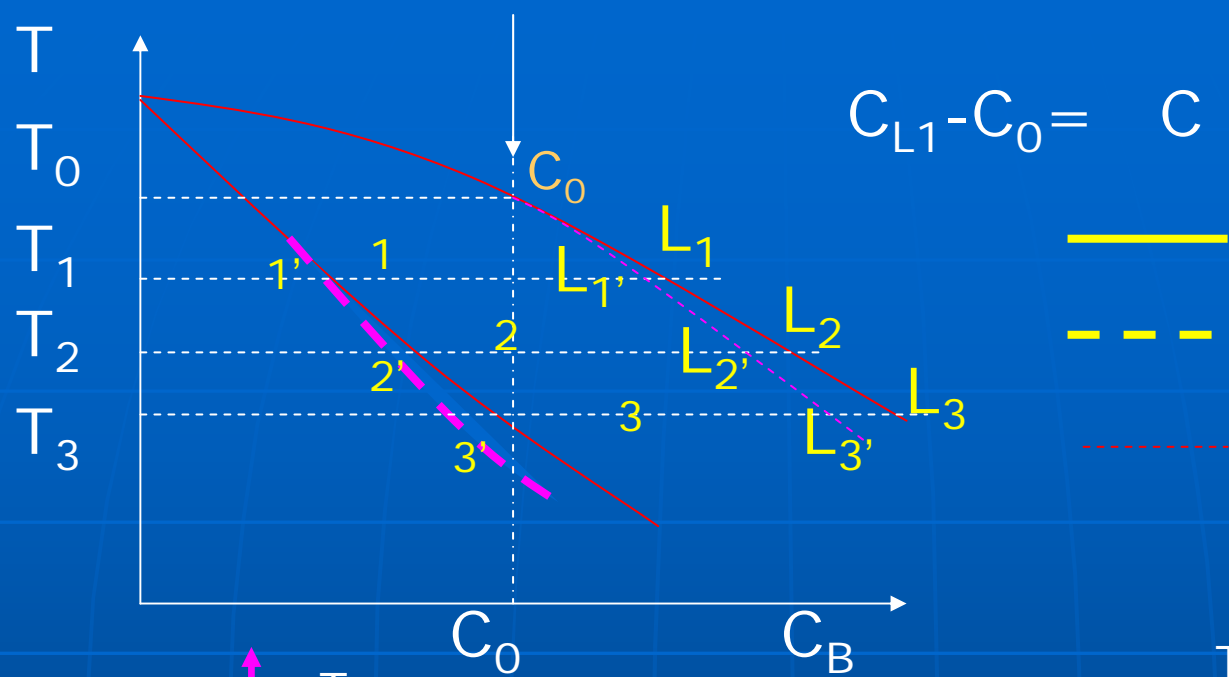
A

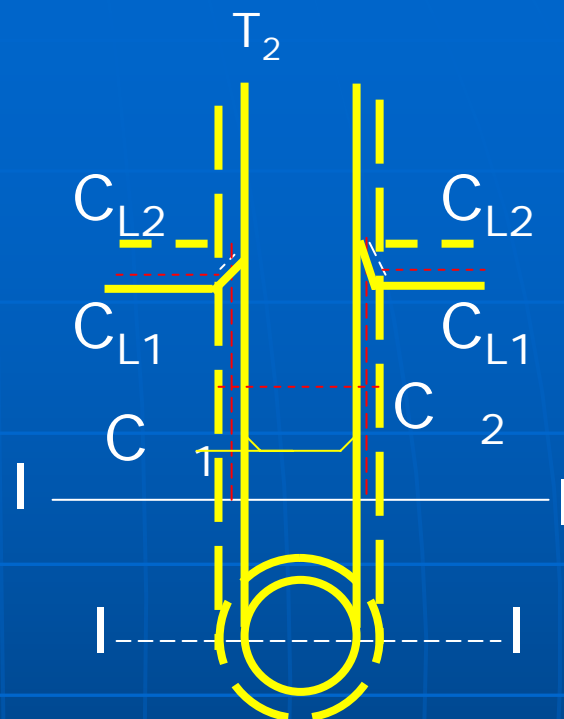
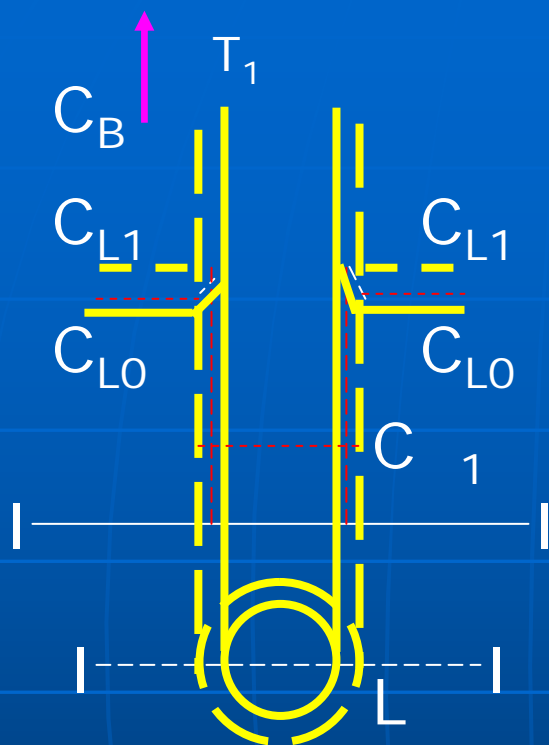
B

C

1.







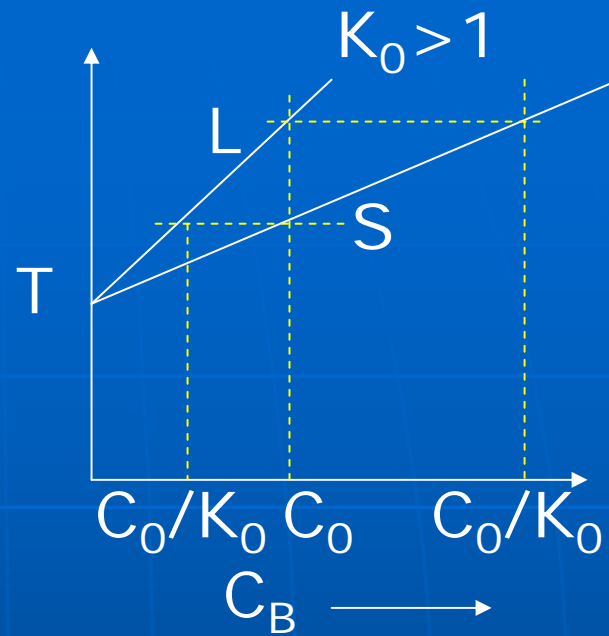
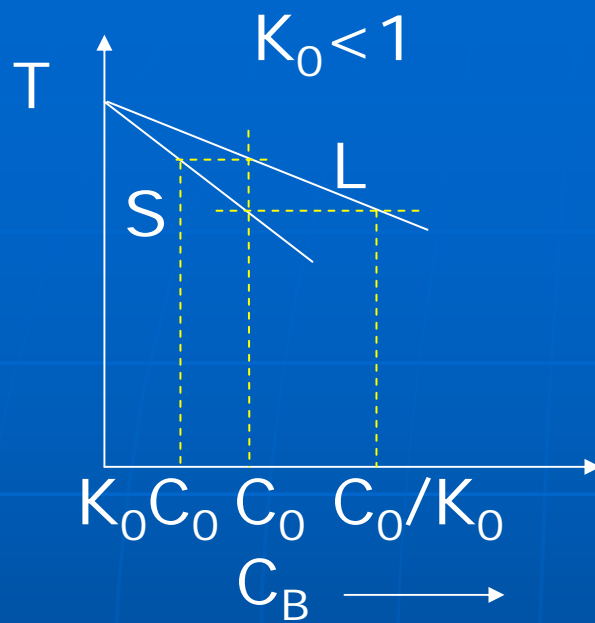
—

- - -

A

.

1.



K_0

(1).

K_0

$K_0 = C_S / C_L$

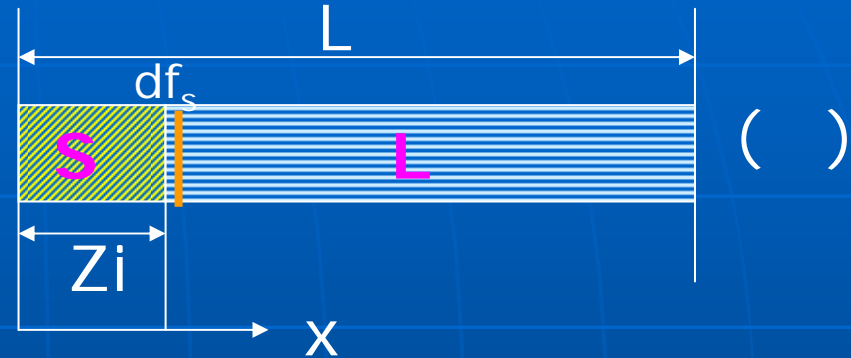
(2).

$C_S = K_0 C_L$

(3).

2. 液相内容质可充分均匀混合

$$f_S = Z_i / L$$



$$(C_L - C_S)df_s = (1 - f_s - df_s)dC_L$$

$$(C_L - K_0 C_L)df_s = (1 - f_s)df_s - df_s dC_L,$$

$$dC_L / C_L = (1 - k_0)df_s / (1 - f_s),$$

$$\ln C_L = (k_0 - 1) \ln(1 - f_s) + \ln C$$

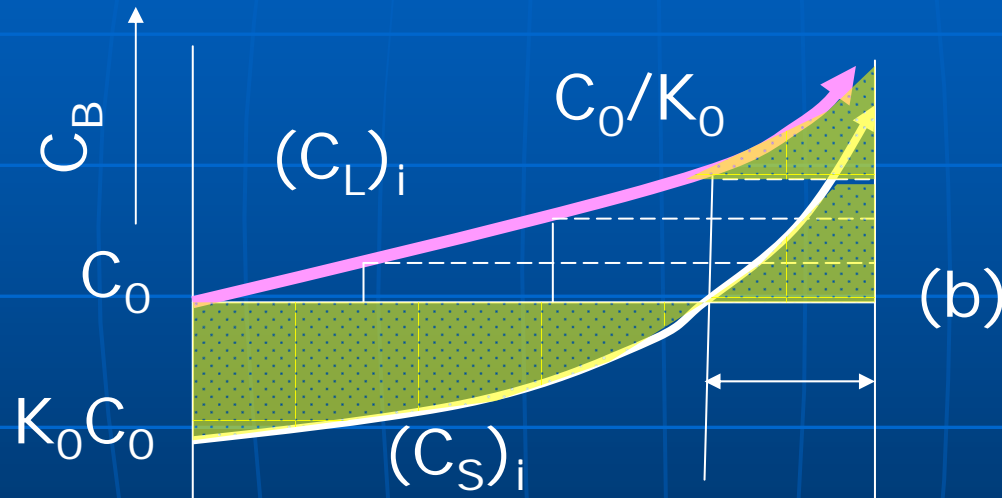
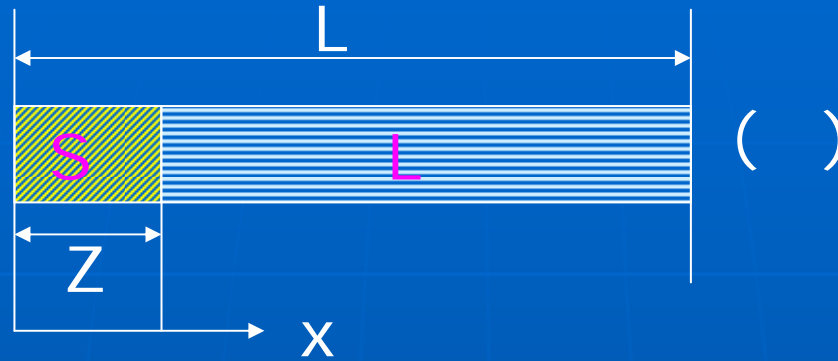
$$f_s = 0$$

$$C_L = C_0,$$

$$C = C_0$$

$$C_L = C_0 (1 - f_s)^{(K_0 - 1)} = C_0 f_L^{(K_0 - 1)}$$

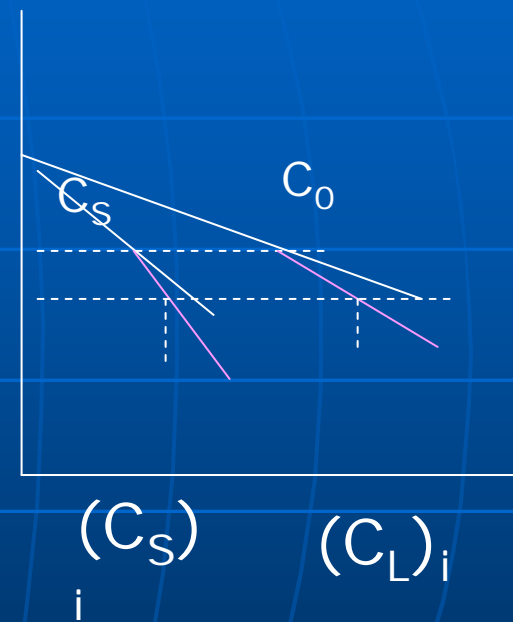
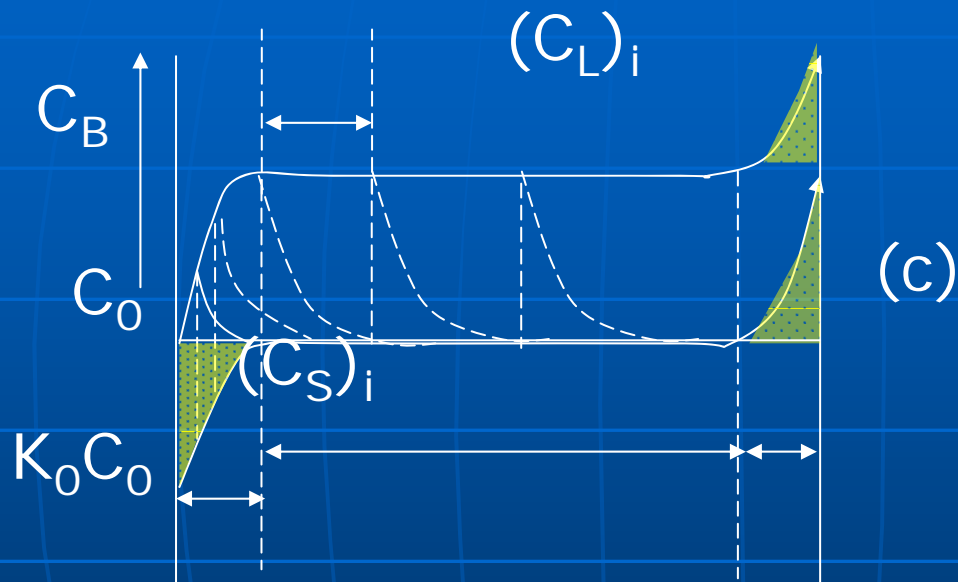
$$C_S = K_0 C_0 (1 - f_s)^{(K_0 - 1)}$$



$$C_L = C_0(1 - fs)^{(K_0 - 1)} = C_0 f_L^{(K_0 - 1)}$$

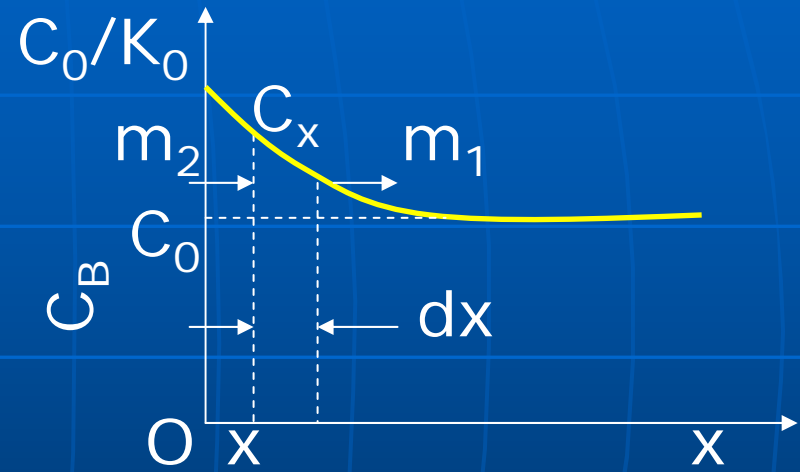
$$C_S = K_0 C_0(1 - fs)^{(K_0 - 1)}$$

3. 液相内容质仅靠扩散混合



“

”



(m x)

(1).

$$\frac{dm_1}{dx} = -D \frac{d^2 C_x}{dx^2}$$

(2).

$$R \cdot \frac{\partial C_L}{\partial x}$$

$$\frac{d^2 C_x}{dx^2} = -DR \cdot \frac{\partial C_L}{\partial x}$$

$$C_x = B e^{-\frac{Rx}{D}} + A$$

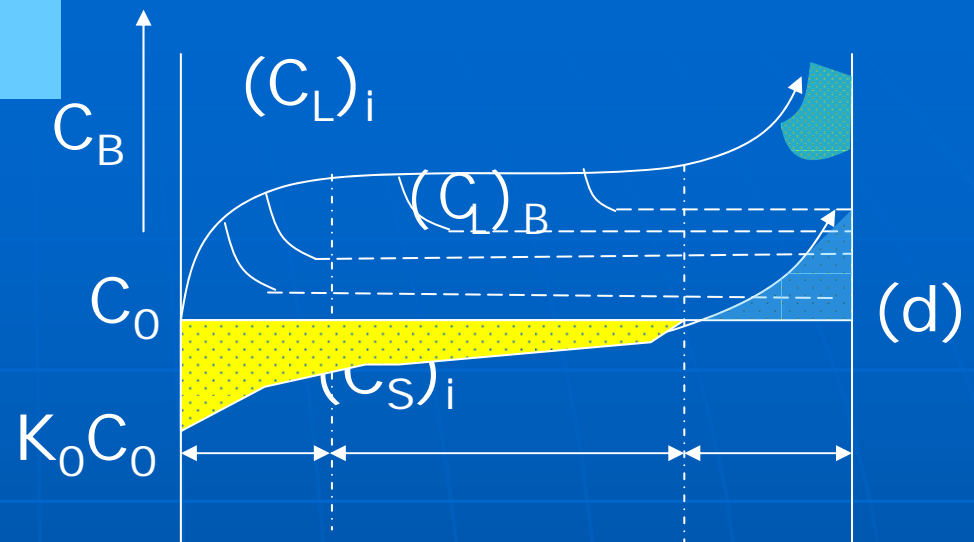
$$X=0 \quad C_L = C_0/K_0 = A+B. \quad B = C_L - A$$

$$x \quad , \quad C_L = C_0, \quad B = C_0/K_0 - C_0$$

$$C_x = C_0 \left[1 + \frac{1-K_0}{K_0} \exp\left(-\frac{Rx}{D}\right) \right]$$

4. 液相内溶质部分混合

(1).



(2).

$$dm_1 / dx = -Dd^2C_x / dx^2$$

$$C_x = C_0 \left[1 + \frac{1 - K_0}{K_0} \exp \left(- \frac{Rx}{D} \right) \right]$$

$$(C_L)_i \quad (C_L)_B$$

$$(C_L)_i / (C_L)_B$$

$$K_e = K_0 K_1 = [(C_S)_i / (C_L)_i] \bullet [(C_L)_i / (C_L)_B] = (C_S)_i / (C_L)_B$$

$$K_0$$

$$K_e = K_0 / \left[K_0 + (1 - K_0) e^{-R\delta / D} \right]$$

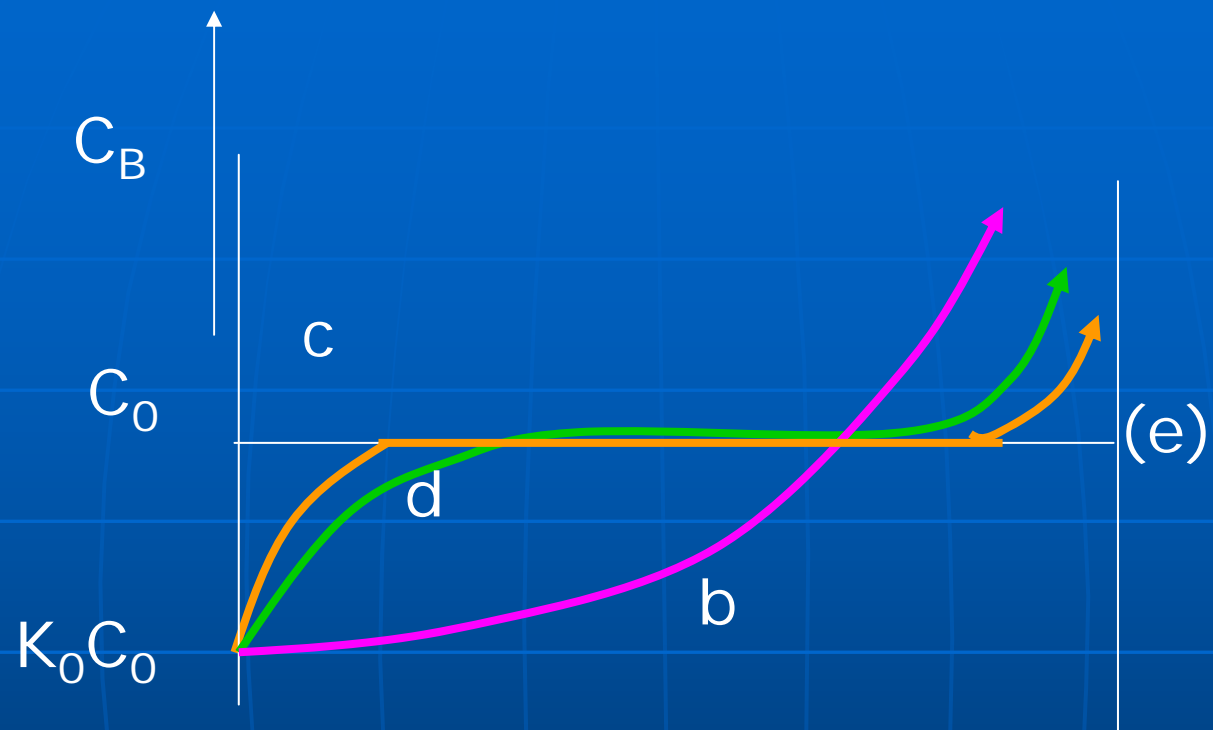
$$(C_L)_B = C_0(1 - Z/L)^{K_e - 1} = C_0(1 - fs)^{K_e - 1}$$

$$C_S = K_e C_0(1 - Z/L)^{K_e - 1} = K_e C_0(1 - fs)^{K_e - 1}$$

$$(1). \quad R \quad 0 \quad K_e = K_0$$

$$(2). \quad R = m \times K_e = 1$$

$$(3). \quad K_0 < K_e < 1$$



.

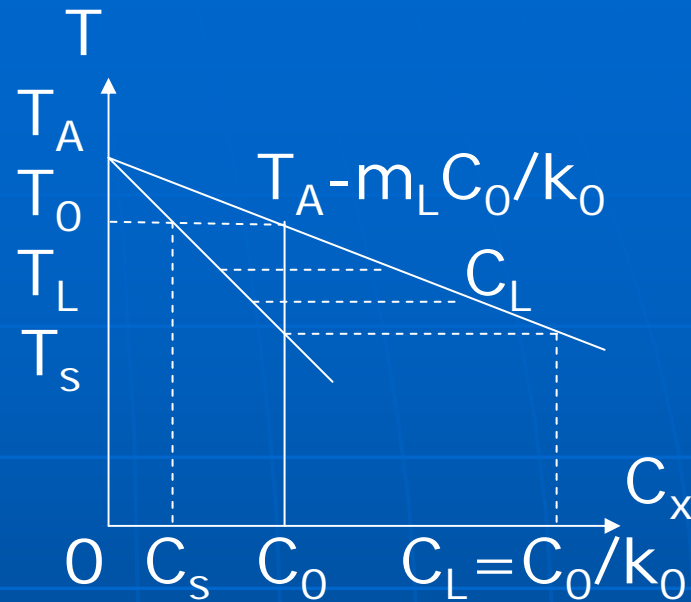
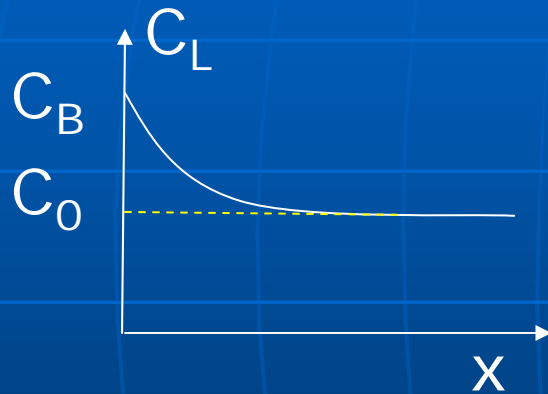
1.

$$T_m$$

2.

$$T_L = T_A - m_L C_L, m_L \quad x = 0$$

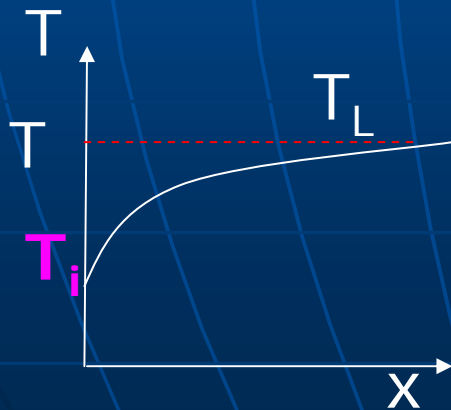
$$C_L = C_0 \left(1 + \frac{1 - k_0}{k_0} e^{-Rx/D} \right), C_L = C_0 \left(\frac{k_0 + 1 - k_0}{k_0} \right) = \frac{C_0}{k_0}$$



$$T_L = T_A - m_L C_0 \left(1 + \frac{1 - k_0}{k_0} e^{-Rx/D} \right)$$

1

$x=0,$



$$\begin{aligned} T_i &= T_A - m_L C_0 \left(1 + \frac{1 - k_0}{k_0} \right) \\ &= T_A - m_L C_0 \frac{k_0 + 1 - k_0}{k_0} = T_A - m_L \frac{C_0}{k_0} \end{aligned}$$

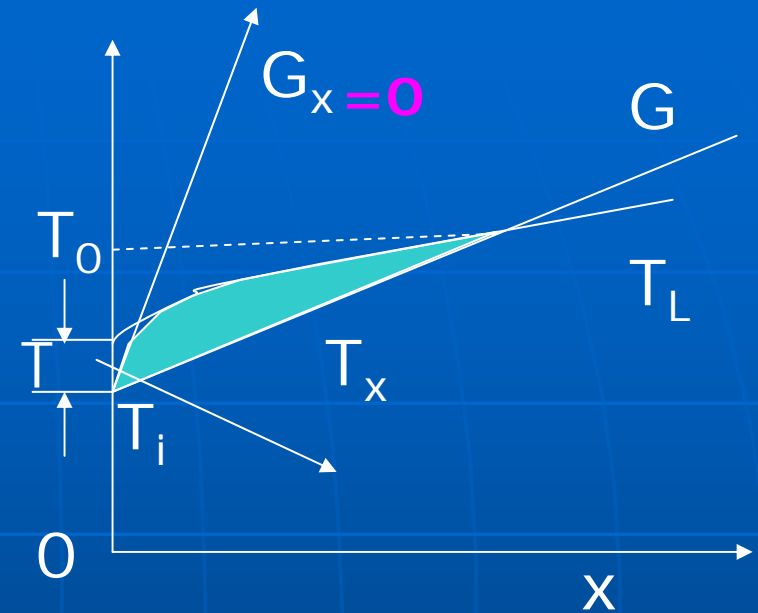
G

$$T_x = T_i + Gx$$

$$= T_A - m_L \frac{C_0}{k_0} + Gx$$

(1)

T_L

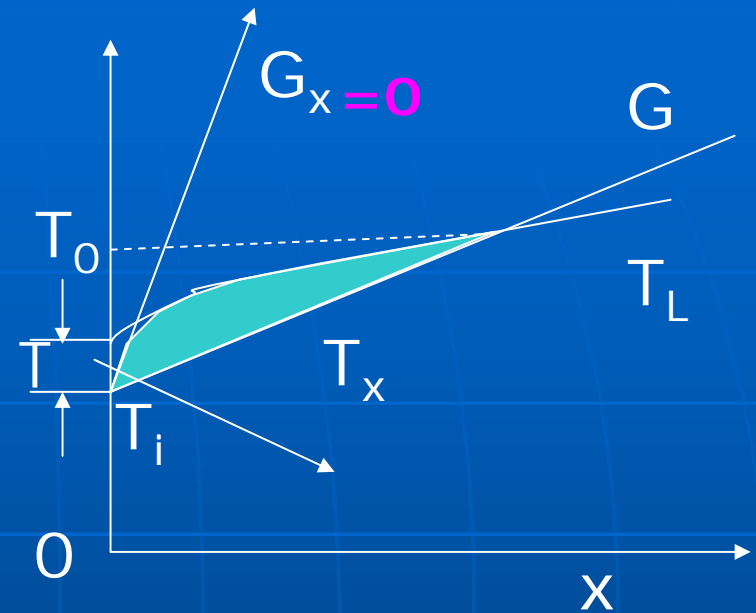


$$\frac{dT_L}{dx} = -\frac{m_L C_0 (1-k_0)}{k_0} \cdot \left(-\frac{R}{D}\right) \cdot e^{-Rx/D},$$

$$x=0 \quad \left. \frac{dT_L}{dx} \right|_{x=0} = \frac{m_L C_0}{D} \cdot \frac{1-k_0}{k_0} R$$

曲线 T_L 斜率大于 G ,
则出现组分过冷, 即

$$\frac{m_L C_0}{D} \cdot \frac{1 - K_0}{K_0} \geq \frac{G}{R}$$



D :

K_0

C_0 :

m_L :

G :

R

G

R

T_L

G

$$\frac{m_L C_0}{D} \frac{1 - k_0}{k_0} \geq \frac{G}{R}$$

$\left\{ \begin{array}{l} G \\ R \end{array} \right.$

$\left\{ \begin{array}{l} G \\ R \end{array} \right.$

$\left\{ \begin{array}{l} D \\ K_0 \end{array} \right.$

C_0

m_L

.

1.

(1).

(2).

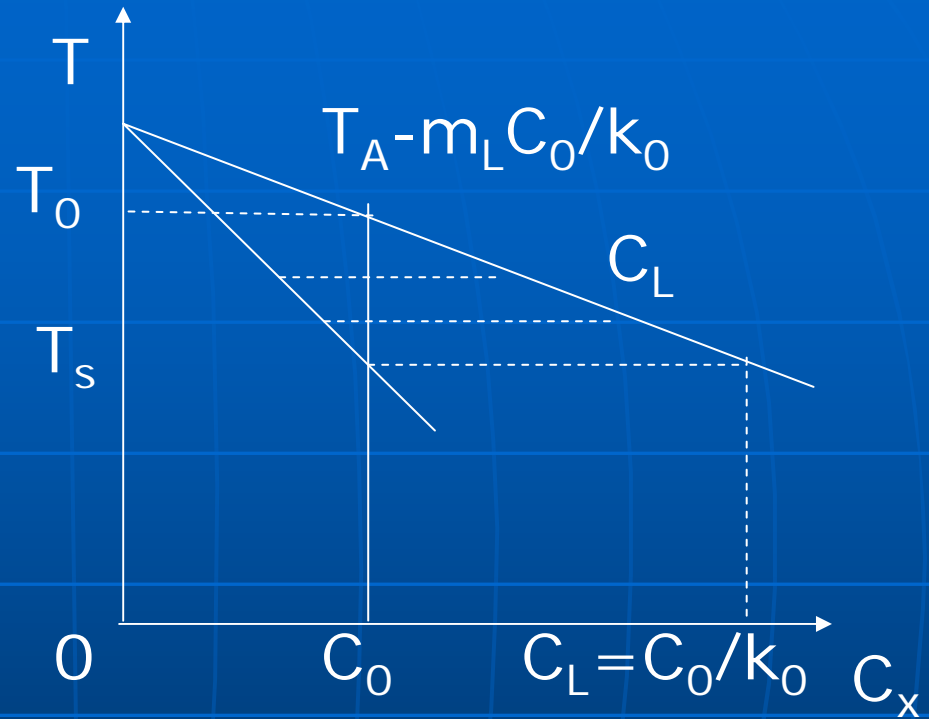
$$G/R \geq m_L C_0 (1 - k_0) / D k_0$$

2.

(1). ()

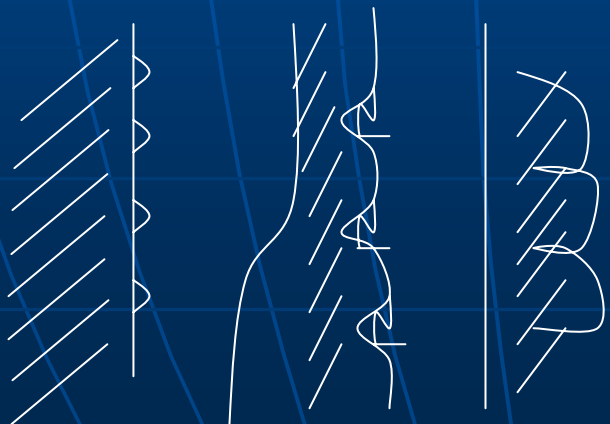
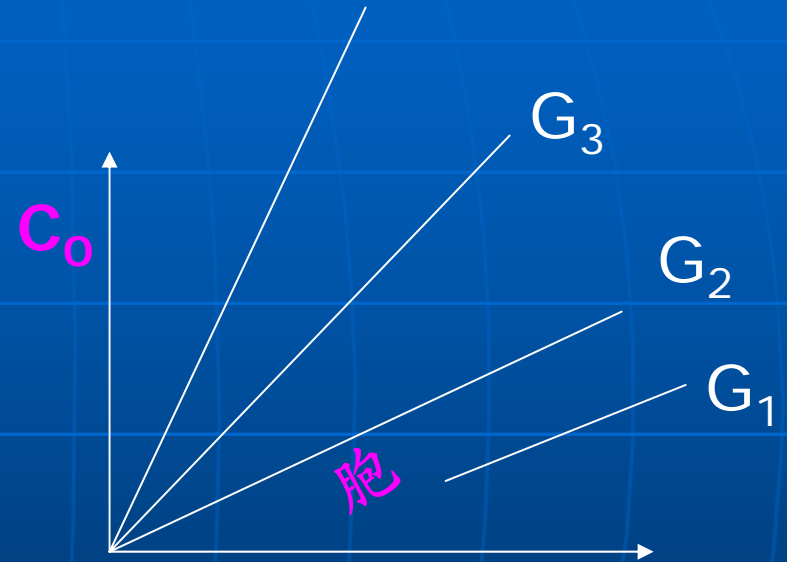
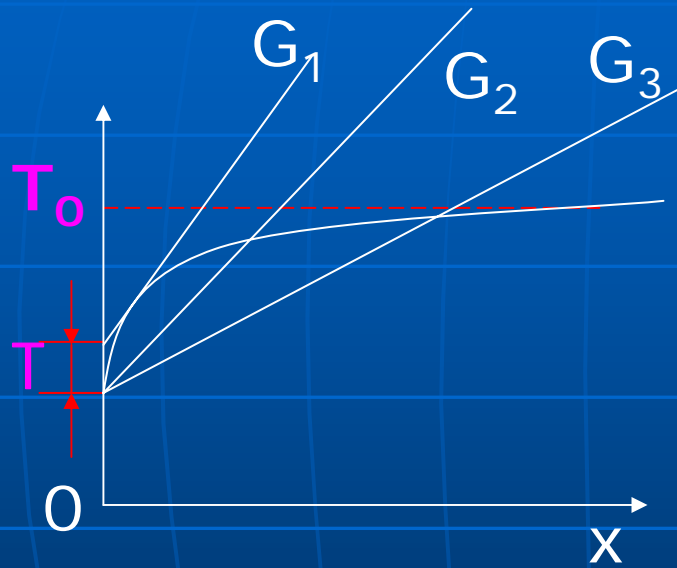
$$\frac{m_L C_0}{D} \frac{1-k_0}{k_0} \geq G/R$$

$$m_L = \frac{T_0 - T_s}{C_L - C_0} = \frac{T_0 - T_s}{C_0 \left(\frac{1}{k_0} - 1 \right)} = \frac{\Delta T_C}{C_0 \frac{1-k_0}{k_0}}$$



$$G/R \geq \frac{\Delta T_{C_0}}{D}$$

(2).



G/R